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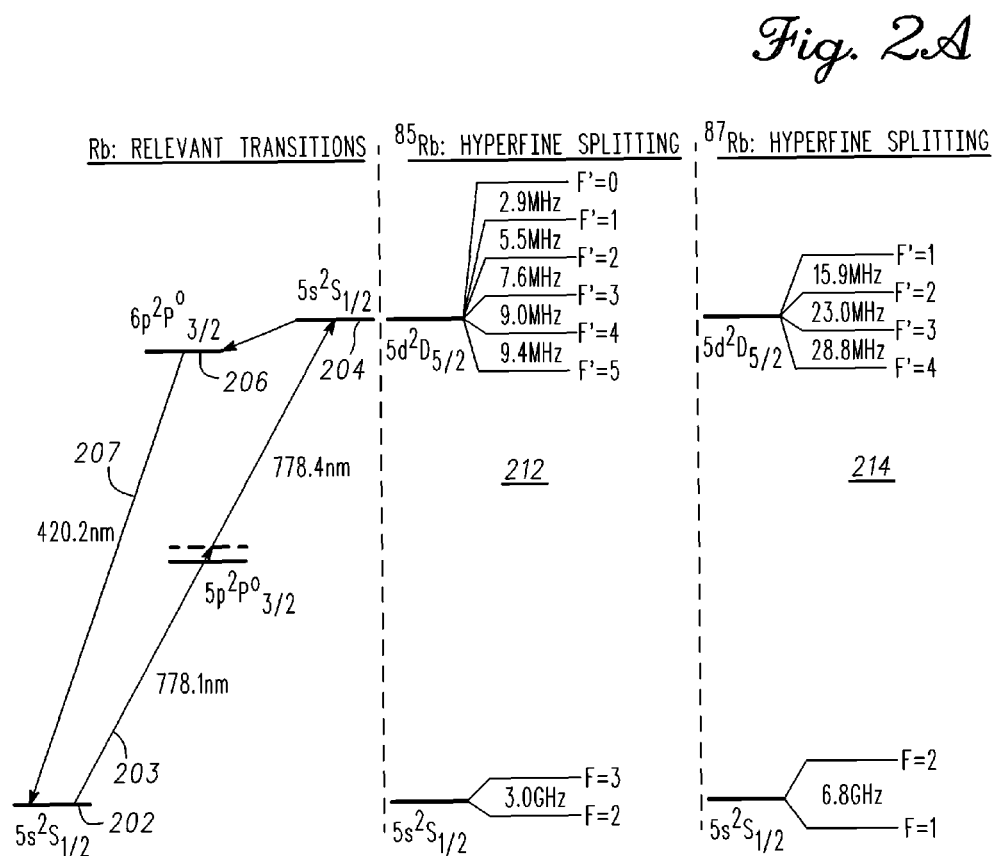
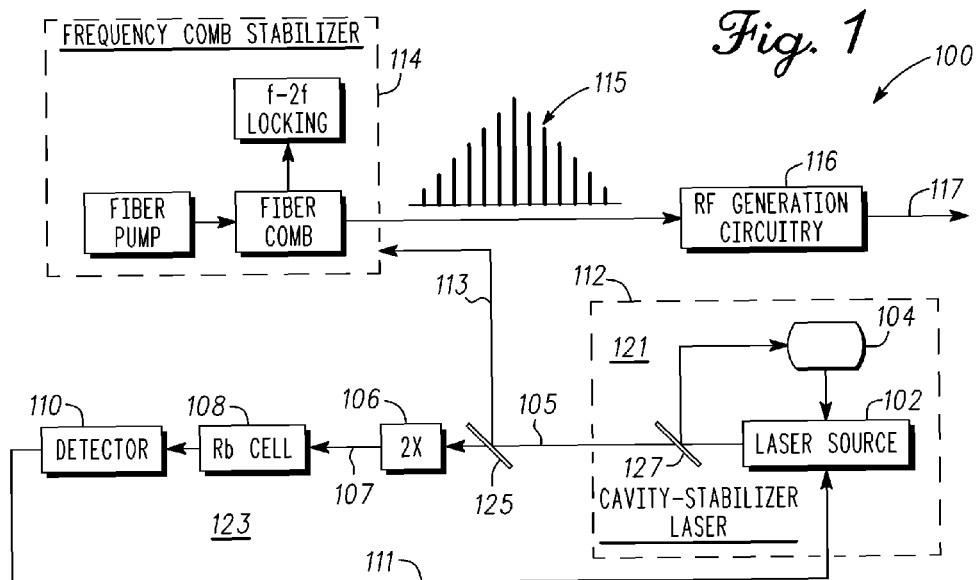
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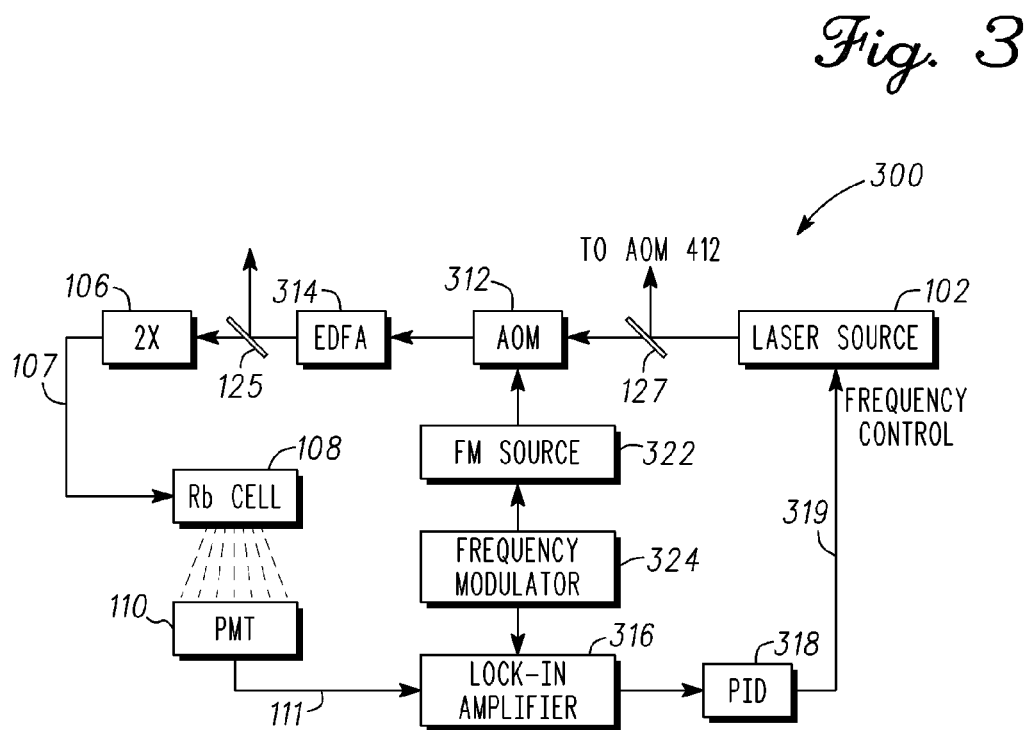
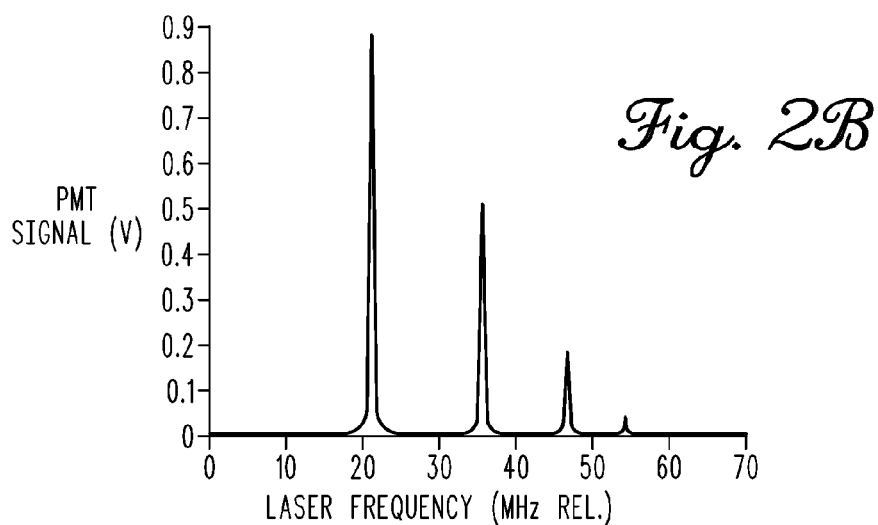
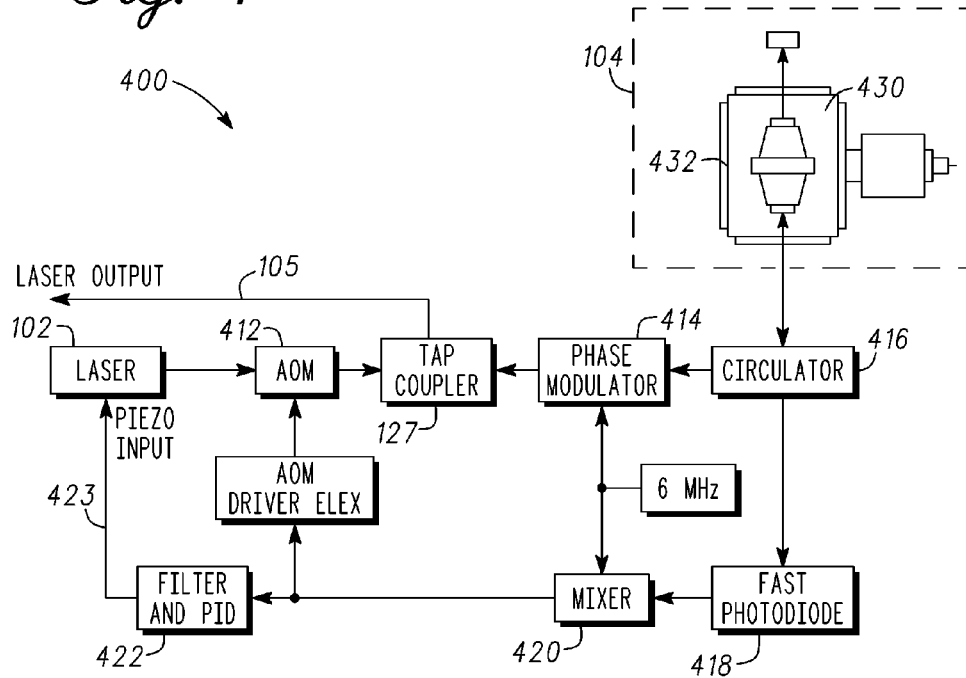
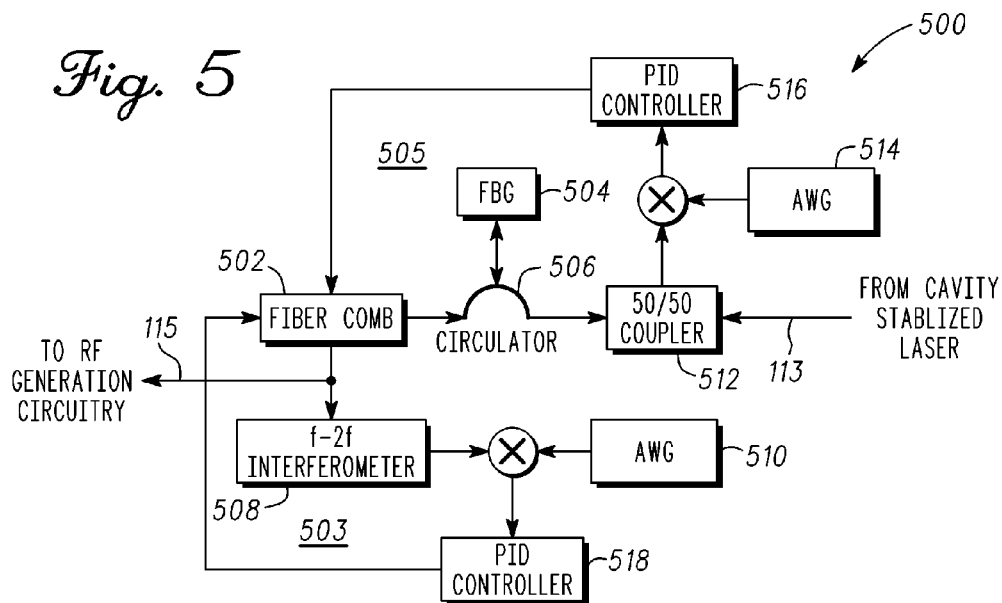
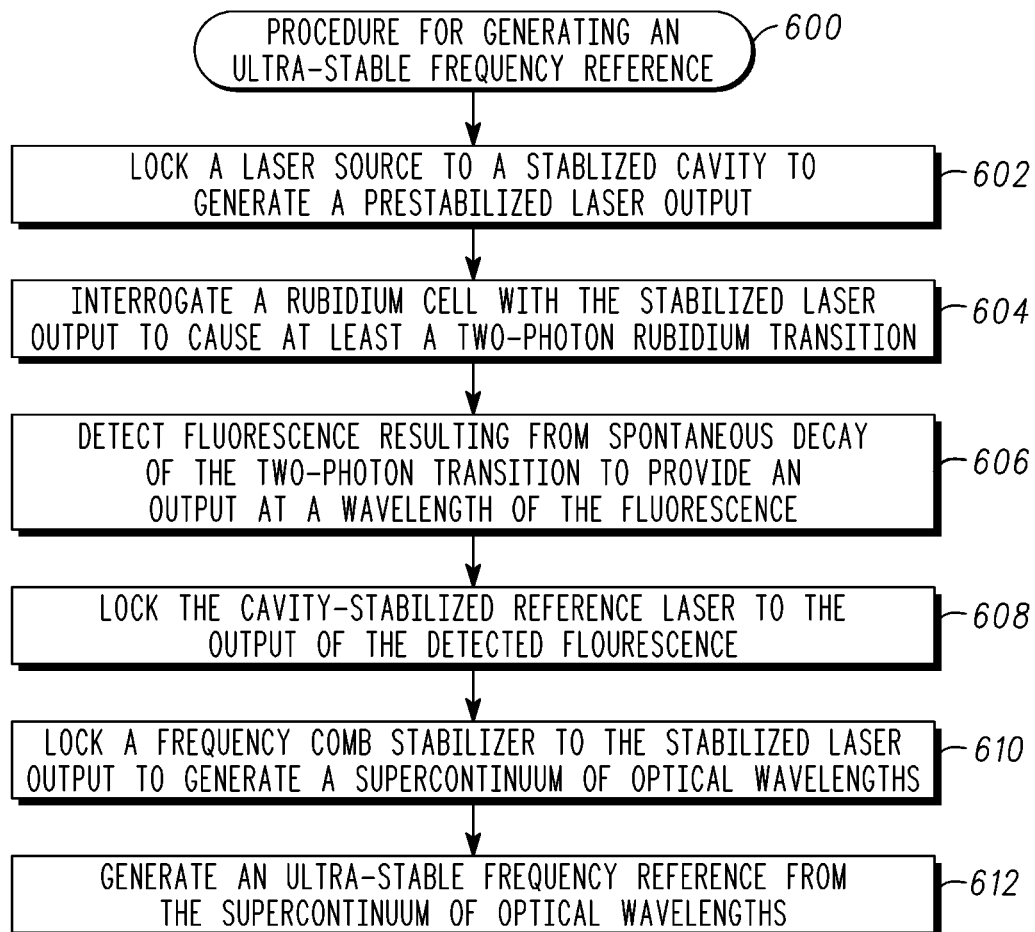


Fig. 4*Fig. 5*

*Fig. 6*

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**PRECISION PHOTONIC OSCILLATOR AND
METHOD FOR GENERATING AN
ULTRA-STABLE FREQUENCY REFERENCE
USING A TWO-PHOTON RUBIDIUM
TRANSITION**

CLAIM OF PRIORITY

This patent application is a continuation of U.S. patent application Ser. No. 13/400,348 entitled "PRECISION PHOTONIC OSCILLATOR AND METHOD FOR GENERATING AN ULTRA-STABLE FREQUENCY REFERENCE USING A TWO-PHOTON RUBIDIUM TRANSITION" filed Feb. 20, 2012, the entire contents of which are hereby incorporated in its entirety.

GOVERNMENT RIGHTS

This invention was not made with United States Government support. The United States Government does not have certain rights in this invention.

TECHNICAL FIELD

Embodiments pertain to precision oscillators and the generation of ultra-stable frequency references. Some embodiments relate to photonic oscillators. Some embodiments relate to frequency reference generation and communication systems. Some embodiments relate to low-phase noise ultra-stable oscillators for radar systems and airborne systems.

BACKGROUND

One issue with many conventional frequency references is stability. Conventional techniques for reaching frequency stabilities (i.e., $\Delta f/f$) in the range of 10^{-14} or better use cryogenically cooled crystal oscillators, cesium fountain clocks, and/or highly stabilized optical clocks. Many of these conventional frequency references are not attractive due to their large size, weight, complexity and/or power consumption.

Thus, there are general needs for improved precision oscillators and methods for generating ultra-stable frequency references. There are also general needs for precision oscillators and methods for generating ultra-stable frequency references that are less complex than many conventional systems. There are also needs for low-phase noise and ultra-stable oscillators that are suitable for use in radar systems, communication systems and signal-collection systems. There are also needs for ultra-stable oscillators for use in systems that require synchronization. There are also needs for ultra-stable oscillators suitable for use in difficult EMI environments. There are also needs for an ultra-stable frequency reference that can provide a frequency stability that exceeds 10^{-14} .

SUMMARY

In some embodiments, an ultra-stable frequency reference generating system include a cavity-stabilized reference laser comprising a laser source locked to a stabilized cavity to generate a stabilized laser output, a Rubidium cell configured to be interrogated by the stabilized laser output to cause at least a two-photon Rubidium transition, and a detector to detect fluorescence resulting from the spontaneous decay of this upper state Rubidium transition. The detector may provide an output at the wavelength of the fluorescence to lock the cavity-stabilized reference laser to generate a stabilized

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laser output. A frequency comb stabilizer may be included to lock to the stabilized laser output to generate a super-continuum of optical wavelengths for use in generating an ultra-stable frequency reference covering a broad spectral range.

In some embodiments, an ultra-stable frequency reference generating system is provided that includes a cavity lock loop to lock a laser source to a stabilized cavity and generate a pre-stabilized laser output and a frequency control loop to further lock the laser source to a decay of an upper state Rubidium transition using two photon excitation to generate a stabilized laser output. The system may also include a frequency comb stabilizer having a first frequency comb stabilizer control loop to stabilize a frequency comb relative to zero frequency and a second frequency comb stabilizer control loop to stabilize the frequency comb spacing. The frequency comb may be a femtosecond frequency comb.

In some embodiments, a method to generate an ultra-stable frequency reference is provided. In these embodiments, a laser source is locked to a stabilized cavity to generate a pre-stabilized laser output. The laser source is further locked to the decay of a two-photon Rubidium transition to generate a stabilized laser output. A frequency comb stabilizer is locked to the stabilized laser output to generate an optical output for use in generating an ultra-stable frequency reference.

BRIEF DESCRIPTION OF THE DRAWINGS

The claims are directed to some of the various embodiments disclosed herein. However, the detailed description presents a more complete understanding of the various embodiments when considered in connection with the figures, wherein like reference numbers refer to similar items throughout the figures.

FIG. 1 is a functional diagram of an ultra-stable frequency reference generating system in accordance with some embodiments;

FIG. 2A illustrates Rubidium transitions in accordance with some embodiments;

FIG. 2B illustrates a sample spectrum of hyperfine transitions that may be used as frequency references in accordance with some embodiments;

FIG. 3 illustrates a frequency control loop for an ultra-stable frequency reference generating system in accordance with some embodiments;

FIG. 4 illustrates a cavity lock loop for an ultra-stable frequency reference generating system in accordance with some embodiments;

FIG. 5 illustrates a frequency comb stabilizer for an ultra-stable frequency reference generating system in accordance with some embodiments; and

FIG. 6 is a procedure for generating an ultra-stable frequency reference in accordance with some embodiments.

DETAILED DESCRIPTION

The following description and the drawings sufficiently illustrate specific embodiments to enable those skilled in the art to practice them. Other embodiments may incorporate structural, logical, electrical, process, and other changes. Portions and features of some embodiments may be included in, or substituted for, those of other embodiments. Embodiments set forth in the claims encompass all available equivalents of those claims.

FIG. 1 is a functional diagram of an ultra-stable frequency reference generating system in accordance with some embodiments. Ultra-stable frequency reference generating

system **100** may be configured to generate an ultra-stable frequency reference **117** having a frequency stability exceeding 5×10^{-14} . In some embodiments, the ultra-stable frequency reference generating system **100** may generate an ultra-stable frequency reference **117** having a frequency stability on the order of and possibly exceeding 10^{-15} , although the scope of the embodiments is not limited in this respect.

Frequency stability, as used herein, refers generally to frequency variation at one second or with a one second averaging. A frequency stability of 10^{-15} , for example, refers to the standard deviation of a series of frequency measurements within a one second averaging time per measurement.

In some embodiments, the ultra-stable frequency reference generating system **100** may include a cavity-stabilized reference laser **112** that includes a laser source **102** locked to a stabilized cavity **104**. The system **100** may also include a Rubidium (Rb) cell **108** that may be interrogated by a stabilized laser output **105** of the cavity-stabilized reference laser **112** which may cause at least a two-photon Rubidium transition (to an upper state) within the Rubidium cell **108**. A detector **110** may detect fluorescence **109** within the Rubidium cell **108** resulting from the spontaneous decay of the upper state Rubidium transition. In these embodiments, the detector **110** may provide a detector output **111** at a wavelength of the fluorescence to lock the cavity-stabilized reference laser **112** to generate a stabilized laser output **113**. In these embodiments, the laser source **102** is locking to both the stabilized cavity **104** and the Rubidium transition within the Rubidium cell **108**.

In some embodiments, the ultra-stable frequency reference generating system **100** may also include a frequency doubler **106** to double the frequency of the stabilized laser output **105**. The doubled stabilized laser output **107** may be configured to interrogate the Rubidium cell **108** to generate an output for use in locking the laser source **102** to the Rubidium transition.

The ultra-stable frequency reference generating system **100** may also include a frequency comb stabilizer **114**, which may be locked to the stabilized laser output **113**. The frequency comb stabilizer **114** may generate an output of optical wavelengths which may comprise a super-continuum **115** of optical wavelengths. The super-continuum **115** may be an octave span of wavelengths, although the scope of the embodiments is not limited in this respect. In some embodiments, the spacing between the optical comb teeth may be determined by a femto second laser pulse repetition frequency of a femto second laser that may be used to generate the frequency comb.

In some embodiments, the ultra-stable frequency reference generating system **100** may also include RF generating circuitry **116** to generate the ultra-stable frequency reference **117** from the super-continuum **115** of optical wavelengths. The ultra-stable frequency reference **117** may comprise one or more ultra-stable RF or microwave output signals, although the scope of the embodiments is not limited in this respect. The RF generating circuitry **116** may include, among other things, a photo detector to convert the super-continuum **115** of optical wavelengths to the ultra-stable frequency reference **117**. In some embodiments, the ultra-stable frequency reference **117** may comprise a set of RF or microwave signals.

In some embodiments, the frequency comb stabilizer **114** may include, among other things, a fiber pump, an f-2f locking interferometer and a fiber-based frequency comb (i.e., a fiber comb). The fiber-based frequency comb may include non-linear fiber to generate the super-continuum **115** of optical wavelengths. In some embodiments, the frequency comb stabilizer **114** includes a first control loop to stabilize the frequency comb relative to zero frequency and a second con-

trol loop to stabilize the frequency comb spacing. These embodiments are discussed in more detail below.

In some embodiments, the Rubidium cell **108** may be a Rubidium vapor cell comprising various isotopes of Rubidium such as Rubidium 85 and Rubidium 87 although the scope of the embodiments is not limited in this respect. In these embodiments, the Rubidium vapor cell is interrogated (illuminated by an optical source) to cause photon excitation.

As illustrated in FIG. 1, two complementary lock loops may be used to generate the stabilized laser output **113**. A cavity-lock loop **121** may lock the laser source **102** to the stabilized cavity **104**. The cavity-lock loop **121** may help short-term phase noise performance of the system **100**. A frequency control loop **123** may lock the laser source **102** to the Rubidium transition within the Rubidium cell **108**. The frequency control loop **123** may help reduce long-term environmental drift to help achieve longer-term stability. In these embodiments, the frequency control loop **123** may lock the laser source to a decay of an upper state Rubidium transition using two-photon excitation to generate the stabilized laser output.

In these embodiments, by locking the laser source **102** to a stabilized cavity **104**, variation of the laser frequency of the cavity-stabilized reference laser **112** may be reduced. By locking the output of the cavity-stabilized reference laser **112** to an atomic transition (i.e., a two-photon Rubidium transition), the variation of the laser frequency is further reduced. Without the use of any locking loops, the frequency of the laser output may drift by several MHz over the course of a few minutes. Locking to the stabilized cavity **104** may reduce this drift substantially (e.g., by almost a million times or more). Locking to the two-photon Rubidium transition may remove any slow drift that remains. Accordingly, frequency fluctuations and drifts have been removed or at least largely reduced so that the output **113** is considered stabilized.

System **100** may provide significant improvement in long-term stability and phase noise is achieved over many conventional systems. For example, the ultra-stable frequency reference **117** generated by the ultra-stable frequency reference generating system **100** may have a frequency stability of at least 5×10^{-14} or greater, and may even have a frequency stability exceeding 5×10^{-15} , although the scope of the embodiments is not limited in this respect. The ultra-stable frequency reference **117** may further have a phase noise of less than -100 dBc/Hz at one Hz off a 10 GHz carrier, for example.

The ultra-stable frequency reference generating system **100** may be implemented as a chip-scale frequency reference and may provide better performance than many conventional crystal oscillators currently in use in small, inexpensive devices such as handheld GPS receivers. In some embodiments, the ultra-stable frequency reference generating system **100** may be implemented a package suitable for integration into a spacecraft or airborne system.

The ultra-stable frequency reference generating system **100** may be also suitable for use in radar systems, communication systems and signal-collection systems. The ultra-stable frequency reference generating system **100** may also be suitable for use in systems that require synchronization. The ultra-stable frequency reference generating system **100** may also be suitable for use in difficult EMI environments.

Although the ultra-stable frequency reference generating system **100** is illustrated in FIG. 1 as having several separate functional elements, one or more of the functional elements may be combined and may be implemented by combinations of hardware elements and software-configured elements, such as processing elements including digital signal proces-

sors (DSPs), and/or other hardware elements. For example, some elements may comprise one or more microprocessors, DSPs, application specific integrated circuits (ASICs), radio-frequency integrated circuits (RFICs) and combinations of various hardware and logic circuitry for performing at least the functions described herein. In some embodiments, the functional elements of the ultra-stable frequency reference generating system **100** may refer to one or more processes operating on one or more processing elements.

FIG. 2A illustrates Rubidium transitions in accordance with some embodiments. As discussed above, interrogation of the Rubidium cell **108** (FIG. 1) by the stabilized laser output **107** (FIG. 1) may cause at least a two-photon Rubidium transition **203**. The two-photon Rubidium transition **203** may be a two-photon Rubidium transition from the 5s state **202** to the 5d state **204** as illustrated. A spontaneous decay from the 6p state **206** to the 5s state **202**, shown as decay transition **207**, may result in fluorescence that may be detected by detector **110** (FIG. 1). The excited atoms spontaneously decay from an upper state (e.g., state **206**) to a lower state (e.g., state **202**) emitting a fluorescence at a precise wavelength.

In these embodiments, the two-photon Rubidium transition **203** from the 5s state **202** to the 5d state **204** may be at wavelength of precisely 778.1 nm. The decay transition **207** and the detected fluorescence **109** (FIG. 1) may be at a wavelength of precisely 420.2 nm. In these embodiments, the detector output **111** (FIG. 1) may be at the wavelength of the decay transition **207** (e.g., 420.2 nm) and may be used to further lock the cavity-stabilized reference laser **112** (FIG. 1) to generate the stabilized laser output **113** (FIG. 1). In these embodiments, the detector **110** may be selected to be sensitive to the wavelength of the decay transition **207**.

In some example embodiments, the laser source **102** may be a 1556 nm fiber laser that generates a 1556 nm wavelength. When halved by the wavelength divider **106** (FIG. 1), a 778 nm wavelength may be produced which may be used to cause the two-photon transition **203** within the Rubidium cell **108**. In these example embodiments, the 1556 nm fiber laser is used since the two-photon Rubidium transition **203** occurs at precisely 778 nm, which is precisely half of the 1556 nm wavelength. Other laser source and wavelength divider/multiplier combinations may also be used to generate a 778 nm wavelength to cause the two-photon Rubidium transition **203**. In some embodiments, the wavelength divider **106** may comprise non-linear optics to convert the 1556 nm wavelength to a 778 nm wavelength, although this is not a requirement.

FIG. 2A also illustrates hyperfine splitting **212** for Rubidium 85 and hyperfine splitting **214** for Rubidium 87. This hyperfine splitting results in different transitions and may occur for the 5s state **202** and the 5d state **205** as shown. In accordance with some embodiments, the strongest transition in one of the isotopes of Rubidium may be used for stabilization.

In some embodiments, the stabilized cavity **104** (FIG. 1) may be a dimensionally-stable optical cavity and may be an ultra-low expansion (ULE) glass Fabry-Perot cavity, although this is not a requirement. The output of the laser source **102** may be pre-stabilized to the optical cavity using a Pound-Drever-Hall (PDH) stabilization technique. This pre-stabilization may improve the short term stability of the ultra-stable frequency reference generating system **100**. In an example embodiment, a Fabry Perot cavity may be used that has length of 7.75 cm and a high finesse of greater than or equal to 150,000. In some embodiments, a notched mount cavity with finesse of 10,000 may be used, while in other embodiments, a mid-plane mount cavity with finesse of 150,

000 may be used. Although pre-stabilizing the laser source **102** to a high finesse cavity improves its short term frequency stability, at longer times thermal drift of the cavity length may cause unwanted frequency wander. This frequency wander may be removed by locking the frequency of the laser source **102** to the time invariant two-photon Rubidium transition.

FIG. 2B illustrates a sample spectrum of hyperfine transitions that may be used as frequency references in accordance with some embodiments. The sample spectrum of the $5S_{1/2}$ ($F=2$) \rightarrow $5D_{5/2}$ ($F=4, 3, 2, 1$) hyperfine transitions is shown, which includes a spectra of transitions from the $5S_{1/2}$ ground state into the $5D_{5/2}$ excited state. The spectra are transitions in ^{87}Rb from the hyperfine ground state $F=2$ to the hyperfine excited states (from the left) $F=4, F=3, F=2$ and $F=1$ are also shown.

FIG. 3 illustrates a frequency control loop for an ultra-stable frequency reference generating system in accordance with some embodiments. Frequency control loop **300** may be suitable for use as frequency control loop **123** (FIG. 1) to lock the laser source **102** (FIG. 1) to the Rubidium transition **207** (FIG. 2A).

In addition to laser source **102**, the wavelength divider **106**, the Rubidium cell **108** and the detector **110** previously discussed, the frequency control loop **300** may include a modulator such as an acousto-optic modulator (AOM) **312** to modulate the stabilized laser output **105**. The frequency control loop **300** may also include an amplifier such as an erbium-doped fiber amplifier (EDFA) **314** to amplify the modulated output of the AOM **312** prior to coupler **125** which couples wavelengths to the frequency comb stabilizer **114** (FIG. 1). The frequency control loop **300** may also include a lock-in amplifier **316** and a proportional integral derivative (PID) controller **318** to operate on the output signal **111** from the detector and generate an error signal **319** for frequency control of the laser source **102**. An FM source **322** may provide an FM signal to the AOM **312** and may be modulated by frequency modulator **324** that may be used provide a dither on the error signal **319** for the frequency control of the laser source **102**. To generate the error signal **319** used to lock the pre-stabilized reference laser to the frequency of the two-photon resonance in Rubidium, the probe beam may be frequency dithered and the resulting fluorescence may be demodulated using the lock-in amplifier **316**. In some embodiments, the detector **110** may comprise a photo-multiplier tube (PMT).

FIG. 4 illustrates a cavity lock loop for an ultra-stable frequency reference generating system in accordance with some embodiments. Cavity lock loop **400** may be suitable for use as cavity lock loop **121** (FIG. 1) to lock the laser source **102** to the cavity **104**. The use of cavity lock loop **400** may help achieve improved short-term phase noise performance.

The cavity lock loop **400** may include an AOM **412** to compensate for any frequency offset of the stabilized cavity **104** and a tap coupler **127** to couple the stabilized laser output **105** to AOM **312** (FIG. 3). The cavity lock loop **400** may also include a phase modulator **414**, a circulator **416**, a fast photodiode **418**, a mixer **420** and a filter and PID element **422** arranged in a feedback loop to provide a feedback signal **423** to the laser source **102**. In some embodiments, the feedback signal **423** may be provided to a piezo input of the laser source **102** which controls a piezo-actuated mirror.

In some example embodiments, the stabilized cavity **104** may include a ULE cavity **430** that may be provided within a vacuum enclosure **432**. The stabilized cavity **104** may also include acoustic and vibration isolation, although these are not requirements as other techniques for cavity stabilization may be used.

FIG. 5 illustrates a frequency comb stabilizer for an ultra-stable frequency reference generating system in accordance with some embodiments. The frequency comb stabilizer 500 may be suitable for use within the frequency comb stabilizer 114 (FIG. 1) of ultra-stable frequency reference generating system 100 (FIG. 1), although other configurations may also be suitable. The frequency comb stabilizer 500 may generate the super-continuum 115 from the stabilized laser output 113 (FIG. 1). In some embodiments, the super-continuum 115 may, for example, comprise at least an octave span of wavelengths.

As illustrated in FIG. 5, the frequency comb stabilizer 500 includes a first frequency comb stabilizer control loop 503 to stabilize the frequency comb relative to zero frequency, and a second frequency comb stabilizer control loop 505 to stabilize the frequency comb spacing.

The frequency comb stabilizer 500 may include a fiber-based frequency comb 502 that includes a non-linear fiber to generate the super-continuum 115 of optical wavelengths. An interferometer, such as f-2f interferometer 508, may generate a beat tone from the super-continuum 115 for mixing with an output of a waveform generator 510 to provide an input to PID controller 518 to generate a carrier-envelope offset (CEO) frequency as feedback 519 to the fiber-based frequency comb 502 as part of control loop 503.

Control loop 505 may include a 50-50 coupler 512 to combine the stabilized laser output 113 (FIG. 1) with an output of the fiber comb 502 to generate an RF beat tone which may be mixed with an output from a waveform generator 514 to provide an input to PID controller 516. The PID controller 516 may generate feedback for the fiber comb 502. In some embodiments, a fiber-brag grating (FBG) 504 and a circulator 506 may be included in control loop 505 to filter the optical signal and reduce detection noise.

Referring back to FIG. 1, in some embodiments, in addition to a photo detector, the RF generating circuitry 116 may also include a microwave frequency comb to generate multiple microwave signals from the output of the photo-detector. These multiple microwave signals may comprise a set of clock or reference signals and may have a stability approximating the stability of the stabilized laser output 113 (e.g., on the order of 5×10^{-15} to 5×10^{-14} at a one-second average). The multiple microwave signals may correspond to the ultra-stable frequency reference 117 (FIG. 1). In these embodiments, the set of clock or reference signals may be suitable for use as clock signals in a system that uses multiple clock signals having a common reference, although the scope of the embodiments is not limited in this respect. In some embodiments, a set of optical reference signals may be generated which may be used to lock other lasers and/or may be used as a reference for optical sensors.

FIG. 6 is a procedure for generating an ultra-stable frequency reference in accordance with some embodiments. Procedure 600 may be performed by an ultra-stable frequency reference generating system, such as ultra-stable frequency reference generating system 100 (FIG. 1), although other ultra-stable frequency reference generating systems may also be suitable for use in implementing procedure 600.

Operation 602 comprises locking a laser source to a stabilized cavity to generate a pre-stabilized laser output. In some embodiments, the components of cavity-lock loop 121 (FIG. 1) may be used.

Operation 604 comprises interrogating a Rubidium cell with the pre-stabilized laser output to cause at least a two-photon Rubidium transition. In some embodiments, the two-

photon Rubidium transition 203 (FIG. 2A) may result from interrogation of the Rubidium cell 108 (FIG. 1) with a 778.1 nm wavelength.

Operation 606 comprises detecting fluorescence resulting from the spontaneous decay of the two-photon Rubidium transition to provide an output at a wavelength of the fluorescence. The fluorescence may result from the decay transition 207 (FIG. 2A).

Operation 608 comprises locking the cavity-stabilized reference laser to the output of the detected fluorescence generate a stabilized laser output. In some embodiments, the components of the frequency control loop 123 (FIG. 1) may be used.

Operation 610 comprises locking a frequency comb stabilizer to the stabilized laser output to generate a super-continuum of optical wavelengths. Operation 610 may, for example, be performed by frequency comb stabilizer 114 (FIG. 1).

Operation 612 comprises generating an ultra-stable frequency reference from the super-continuum of optical wavelengths. Operation 612 may, for example, be performed by RF generation circuitry 116 (FIG. 1).

In some embodiments, system 100 (FIG. 1) may comprise a photonic oscillator that is referenced to an atomic resonance (i.e., the Rubidium transition). The frequency stability of an oscillator ($\Delta f/f$) that is referenced to an atomic resonance may be fundamentally limited by both the measured Q of the two-photon transition and the signal to noise ratio (SNR) based on the following equation.

$$\frac{\Delta f}{f} = \frac{1}{Q * SNR * \sqrt{\tau}}$$

Q may be defined as the frequency of the transition divided by the measured linewidth of the transition ($\nu/\Delta\nu$) and τ is the averaging time. The measured linewidth may exceed the natural linewidth due to a variety of broadening mechanisms. To minimize broadening, magnetic shielding may be provided around the rubidium cell 108. This may greatly reduce Zeeman broadening resulting in a measured linewidth near the natural width of 350 kHz. In order to increase the signal to noise level, the fluorescence detection may be operated in a shot-noise limited regime which may be achieved by collecting a sizable portion of the 420.2 nm fluorescence, maximizing the frequency doubling process to 778 nm, optimizing the detector for 420.2 nm operation, eliminating stray light, minimizing detector noise such as Johnson noise and operating a clock with a high Rb vapor pressure. The natural linewidth limited Q of the two-photon transition is $Q=2.6 \times 10^9$ and with a practical SNR of 15000 the system stability may be approximately 2.3×10^{-14} in 1 second and approaching 10^{-15} with less than two minutes of integration. To translate this stability into the microwave/RF domain, the system 100 may utilize a compact means to divide down from the optical domain. This may be accomplished using a femto second laser based frequency comb in circuitry 116 (FIG. 1). To transfer the stability from optical to the microwave, the femtosecond frequency comb may be locked to the cavity stabilized laser 112.

The process for stabilizing the fiber-based frequency comb 502 (FIG. 5) to an externally-stabilized reference laser (i.e., laser output 113), as shown in FIG. 5 as the frequency comb stabilizer 500 in which an envelope offset (CEO) stabilization is used. Control loop stabilizes 503 the frequency comb relative to zero frequency. The super-continuum 115 may be generated within the frequency comb 502 through a highly

nonlinear fiber. The super-continuum **115** may fulfill an octave spanning to generate a beat tone between a fundamental portion of the spectrum and the second harmonic of the octave of the fundamental represents the frequency comb offset from zero. This tone is subsequently mixed in a digital phase detector with an RF tone generated from a disciplined arbitrary waveform generator (AWG) **510**. The mixed down signal is feed into PID controller **518** which adjusts the pump power to mode-locked the fiber-based frequency comb **502**.

The other control loop **505** may stabilize the frequency comb spacing. This may be achieved by stabilizing the cavity length of the mode-locked fiber-based frequency comb. In an example embodiment, the spectrum may be initially narrowed from approximately 100 nm to 0.1 nm through the FBG **504**, whose center wave is equal to that of the cavity stabilized laser. This narrowing process may limit the shot noise on the photo detector, which generates the RF beat tone used to stabilize the frequency comb. After narrowing, the frequency comb is coupled with the cavity stabilized laser using the 50-50 coupler **512** which results in an RF beat tone signifying the frequency difference between the comb line and cavity stabilized laser. The RF beat tone may be generated by an InGaAs photo detector, which may be part of the 50-50 coupler **512**. The resulting RF signal may be mixed against a second disciplined AWG **514** in a digital phase detector. The digital phase detector may be capable of generating an error signal over thirty radians of phase excursions, which allows 10x more phase excursions compared to using an analog mixer as a phase detector. The output from the digital phase detector is routed to the PID controller **516**, which generates the error signal for the comb spacing feedback. In some embodiments, the error signal may control a piezo-actuated mirror inside the fiber-based frequency comb with approximately 10 kHz of bandwidth.

Embodiments may be implemented in one or a combination of hardware, firmware and software. Embodiments may also be implemented as instructions stored on a computer-readable storage device, which may be read and executed by at least one processor to perform the operations described herein. A computer-readable storage device may include any non-transitory mechanism for storing information in a form readable by a machine (e.g., a computer). For example, a computer-readable storage device may include read-only memory (ROM), random-access memory (RAM), magnetic disk storage media, optical storage media, flash-memory devices, and other storage devices and media. Some embodiments may be implemented with one or more processors and may be configured with instructions stored on a computer-readable storage device.

The Abstract is provided to comply with 37 C.F.R. Section 1.72(b) requiring an abstract that will allow the reader to ascertain the nature and gist of the technical disclosure. It is submitted with the understanding that it will not be used to limit or interpret the scope or meaning of the claims. The following claims are hereby incorporated into the detailed description, with each claim standing on its own as a separate embodiment.

What is claimed is:

1. An optical system, comprising:

a frequency doubler configured to receive a stabilized laser output, and double a frequency of the stabilized laser output to form a frequency-doubled stabilized laser output;

a Rubidium cell configured to be interrogated by the frequency-doubled stabilized laser output to cause at least a two-photon Rubidium transition;

a detector configured to detect fluorescence resulting from spontaneous decay of the Rubidium transition.

2. The optical system of claim **1**, further comprising:

a laser source configured to generate the stabilized laser output;

wherein the laser source is locked to a stabilized cavity.

3. The optical system of claim **2**,

wherein the stabilized cavity is a dimensionally-stable optical cavity and comprises an ultra-low expansion (ULE) glass Fabry-Perot cavity, and

wherein an output of the laser source is pre-stabilized to the optical cavity using a Pound-Drever-Hall stabilization technique.

4. The optical system of claim **1**, further comprising a frequency comb stabilizer locked to the stabilized laser output to generate an optical output for use in generating an ultra-stable frequency reference.

5. The optical system of claim **4**, wherein the frequency comb stabilizer includes:

a frequency comb;

a first control loop to stabilize the frequency comb relative to zero frequency; and

a second control loop to stabilize a frequency comb spacing of the frequency comb.

6. The optical system of claim **5**,

wherein the frequency comb comprises a fiber-based frequency comb that includes a non-linear fiber, and wherein the fiber-based frequency comb is to generate a super-continuum of optical wavelengths comprising at least an octave span.

7. The optical system of claim **4**,

wherein the frequency comb stabilizer is locked to the stabilized laser output to generate a super-continuum of optical wavelengths for use in generating the ultra-stable frequency reference, and

wherein the detector is configured to provide a detector output at a wavelength of the fluorescence to lock the laser source to generate the stabilized laser output.

8. The optical system of claim **7**, further comprising RF generating circuitry to generate the ultra-stable frequency reference from the super-continuum of optical wavelengths, the ultra-stable frequency reference comprising one or more ultra-stable microwave or RF output signals.

9. The optical system of claim **8**, wherein the RF generating circuitry comprises:

a photo-detector to convert the super-continuum of optical wavelengths to a set of microwave signals; and

a microwave frequency comb to generate a set of microwave clock or reference signals from the output of the photo-detector, the set of microwave clock or reference signals having a stability approximating a stability of the stabilized laser output.

10. The optical system of claim **7**, further comprising optical reference signal generating circuitry to convert the super-continuum of optical wavelengths to a set of optical reference signals.

11. The optical system of claim **1**,

wherein the two-photon Rubidium transition is a two-photon Rubidium transition from a 5s state to a 5d state;

wherein the detected fluorescence results from the spontaneous decay from a 6p state to the 5s state; and

wherein the Rubidium cell is a Rubidium vapor cell comprising Rubidium **87**.

12. A method for generating an ultra-stable frequency reference comprising:

locking a laser source to a stabilized cavity to generate a pre-stabilized laser output;

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further locking the laser source to a decay of a two-photon Rubidium transition to generate a stabilized laser output; and

doubling a frequency of the stabilized laser output to generate a frequency-doubled stabilized laser output.

13. The method of claim 12, further comprising locking a frequency comb stabilizer to the frequency-doubled stabilized laser output to generate an optical output for use in generating an ultra-stable frequency reference.

14. The method of claim 13, wherein locking the frequency comb stabilizer to the stabilized laser output generates a super-continuum of optical wavelengths, and wherein the method further comprises generating the ultra-stable frequency reference from the super-continuum.

15. The method of claim 13, wherein the frequency comb stabilizer comprises a fiber-based frequency comb that includes a non-linear fiber, and

wherein the method comprises generating the super-continuum of optical wavelengths comprising at least an octave span with the fiber-based frequency comb.

16. The method of claim 12, further comprising:

interrogating a Rubidium cell with the pre-stabilized laser output to cause at least the two-photon Rubidium transition to an upper state; and

detecting fluorescence resulting from spontaneous decay of the upper state Rubidium transition to provide a

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detected output at a wavelength of the fluorescence for use in further locking the laser source.

17. An optical system, comprising:

a cavity-stabilized reference laser configured to produce a stabilized laser output;

a frequency doubler configured to double a frequency of the stabilized laser output to form a frequency-doubled stabilized laser output;

a Rubidium cell configured to receive the frequency-doubled stabilized laser output and produce fluorescence; and

a detector positioned to detect the fluorescence.

18. The optical system of claim 17,

wherein the cavity-stabilized reference laser comprises a laser source locked to a stabilized cavity;

wherein the detector directs a detector output to the laser source to lock the cavity-stabilized reference laser.

19. The optical system of claim 17, further comprising:

a frequency comb stabilizer locked to the stabilized laser output and configured to produce a super-continuum of optical wavelengths; and

RF generating circuitry configured to receive the super-continuum of optical wavelengths and generate an ultra-stable frequency reference.

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